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Laser method for dual-wavelength diagnosis and observation of spontaneous conversion of H_2O microparticles to H_2O_2

Mass spectrometry, fluorescence microscopy, and NMR methods are used to study the transformation of aerosol microparticles. A laser dual-wavelength method for microparticle diagnostics has been developed [1], which makes it possible to study in real time the spontaneous transformation of microparticles, for example, H_2O (in the size range from 1 to 20 μm and more) into H_2O_2 particles.

Recently, studies have been published [2, 3, 4], in which the effect of spontaneous conversion of H_2O microparticles into H_2O_2 microparticles by atomizing bulk water has been experimentally studied. Moreover, H_2O_2 production increases with decreasing diameter of H_2O , microdroplets generated in the range of 1 μm to 20 μm . In work [5], an experimental setup was created, including a mass spectrometer, with the help of which it was observed when spraying microdroplets of H_2O spontaneous formation of anion pyridine $\text{C}_5\text{H}_5\text{N}^-$ from a pre-prepared solution of pyridine: water. Moreover, this is the result of the experiment on spraying and formation $\text{C}_5\text{H}_5\text{N}^-$ was confirmed at both Nanjing University and Stanford University. The easy formation of $\text{C}_5\text{H}_5\text{N}^-$ in water microdroplets provides a direct route for green chemistry to synthesize chemicals. It can be noted that the chemistry of aqueous microdroplets is at the stage of active development. Let us give some examples that confirm this: the reduction of chlorogold acid ($\text{H}[\text{AuCl}_4]$) to gold nanoparticles [6], the reduction of a number of different carboxylic acids and the formation of hydrogen peroxide [2, 7]. No unambiguous theoretical explanation for such a phenomenon exists yet, but certainly points to the unique chemistry of aerosols occurring at the air-water interface.

In this paper discusses a new laser method for two-wave diagnostics of moving aerosol microparticles, which allows observing their spontaneous transformations in real time, for example, H_2O into H_2O_2 .

A variant of construction of the sensing scheme of a laser dual-wavelength microparticle analyzer (LDAM) with symmetric reception of forward or backward scattered radiation with respect to two planes: the plane of two sensing beams OXZ and the plane OYZ located perpendicular to the plane OXZ and passing through the scheme axis OZ is considered. In this so-called axisymmetric two-frequency LDAM scheme, in which the frequency difference of the two probing beams is Ω_m , receiving optics axis OZ_3 coincides with the optical axis of the circuit OZ , and the scattered radiation is received in the spatial region of reception limited by the aperture of the diaphragm having two axes of symmetry OX_3 and OY_3 (see Fig. 1, where the OY_3Z_3 plane coincides with the OXZ plane and the OY_3Z_3 plane coincides with the OYZ plane) [8]. One of the variants of the design of the receiving diaphragm, providing axisymmetric reception, is, for example, a diaphragm with a cross-shaped opening,

located in such a way that one of the slit-shaped openings of this diaphragm is oriented along the axis OX_3 , and the other slit-shaped hole - along the axis OY_3 . If the LDA sounding and reception scheme uses beams of equal intensity, having linearly matched polarizations with the direction of oscillation of the electric vectors in the OYZ plane, then, for example, when receiving forward-scattered radiation within a slit-shaped diaphragm oriented along the OY_3 axis, a high level of amplitude and phase matching is observed, and when receiving radiation within another slit-shaped opening of the diaphragm oriented along the OX_3 axis, a high level of polarization matching of the mixed scattered beams is observed. Depending on the conditions of microparticle flow diagnostics, it is always possible to select such cross-shaped diaphragm sizes that ensure a high level of photocurrent modulation depth and signal-to-noise ratio.

A theoretical model of an axisymmetric LDAM design is considered, which uses a diaphragm with a circular opening located at a distance r_0 from the center of measurement. When receiving forward scattered radiation, the position of the center of symmetry of the diaphragm O_p determined by angles $\theta = \gamma/2$, $\varphi_0 = 0$, and when receiving backscattered radiation – by angles $\theta_0 = 180^\circ + \frac{\gamma}{2}$, $\varphi_0 = 180^\circ$ (Fig. 1).

It should be noted that in the considered scheme of LDAM probing at symmetric reception of backscattered radiation the function of focusing and collecting lenses is performed by one lens, which allows to simplify considerably the layout of LDAM optical block and its alignment. Previously, in [8], the symmetry properties of the spatial structure of the Doppler signal relative to the OXZ and OYZ planes were considered for different polarization states of the probing beams. These symmetry properties should also be taken into account when analyzing the high-frequency signal parameters of the axisymmetric LDAM circuit. In addition, the following properties of the symmetry of the spatial structure of the high-frequency LDAM scheme should also be taken into account, when two probing beams of equal intensity have elliptical polarizations with the same azimuths and ellipticity, or the probing beams have right-handed (left-handed) polarizations, or two beams are linearly polarized and have equal azimuths. In this case, for two arbitrary directions of reception of axisymmetrical relative to the OZ axis of the scheme, the elementary high-frequency signals are phase-conjugate and have equal amplitudes, as well as equal values of the polarization and amplitude matching coefficients. This is the so-called second type of symmetrical reception of scattered radiation [9].

The noted properties of the symmetry of the spatial structure of the useful high-frequency signal allow, when calculating the parameters of this signal for the LDAM scheme with axisymmetric reception of scattered radiation, in a finite angular aperture, to neglect the interference terms of the low-frequency component of the signal, as well as the high-frequency components of the signal formed from mutually orthogonal components of the corresponding probing beams, since they are equal to zero [12]. As for the remaining high-frequency components of the signal, arising respectively from “x” and “y” – the components of two probing beams, then when determining them in this case it is sufficient to calculate the integrals within one quarter of the diaphragm, i.e. the integration boundaries for ε are taken within the range from $\varepsilon = 0$ to $\varepsilon = \frac{\pi}{2}$, followed by multiplying the resulting signal value by four.

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