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¹V. M. Kondratiuk,
²S. I. Ilnytska,
³O. V. Kutsenko,
⁴O. A. Sushchenko,
⁵M. V. Kondratiuk,
⁶O. V. Semenenko

EXPERIMENTAL RESEARCH OF INTEGRATED NAVIGATION SYSTEMS IN PROBLEMS OF QUADROTOR PATH TRACKING

^{1,2,3,5,6}Research and Training Centre “Aerospace Centre,” National Aviation University, Kyiv, Ukraine

⁴Faculty of Air Navigation, Electronics and Telecommunications, National Aviation University, Kyiv, Ukraine

E-mails: ¹kon_vm@ukr.net ORCID 0000-0002-5690-8873, ²ilnytskasv84@gmail.com
 ORCID 0000-0003-2568-8262, ³kutsenko@bigmir.net ORCID 0000-0003-2741-5559, ⁴sushoa@ukr.net
 ORCID 0000-0002-8837-1521, ⁵kondratyukmv@gmail.com ORCID 0000-0003-3376-4800,
⁶sashka_com@ukr.net ORCID 0000-0003-3184-8170

Abstract—The article deals with experimental research of the integrated navigation, guidance, and control system of quadrotor. The mathematical grounds of the study of the system are represented. Algorithm of functioning the integrated system is represented. Equations of the optimal estimation are given. Features of tested equipment are described. The quadrotor trajectory in the horizontal plane is simulated. Coordinates of the topocentric reference frame are researched. The results of the experimental test are shown. The components of velocity are represented. The graphical dependences on the yaw, pitch, and roll are shown. The obtained results can be useful for creating perspective navigation systems for quadrotors. They allow to improve the quality of quadrotor navigation.

Index Terms—Global navigation satellite system; inertial navigation system; guidance and control system; quadrotor; experimental research; flight test.

I. INTRODUCTION AND PROBLEM STATEMENT

Unmanned aerial vehicles (UAVs) or drones are characterized by low cost and ease of operation, which leads to broad prospects for their use for remote sensing, mapping, monitoring and other civilian applications [1] – [4].

However, the complex conditions of their operation and the peculiarities of their application require solving the problems of ensuring high accuracy of trajectory control and stabilization during stochastic and deterministic perturbations. These functions are carried out by the integrated navigation, guidance, and control system.

It is impossible to design such a system without system analysis. System analysis of complex systems represents integration of mathematical, statistical, experimental and other methods [5] – [9].

The aim of this paper is to present some results of testing an integrated navigation, guidance and control system for the quadrotor.

Relatively simple trajectory is selected here for validation, consisting of linear segments, 90-degree turns, climb and descent during straight segment flight.

II. MATHEMATICAL BACKGROUND

This article presents an option of integrated navigation system, where an inertial navigation system (INS) is corrected by Global Navigation Satellite System (GNSS), barometric altimeter and magnetometer. The quaternion $\delta q(t_i)$ representing a small turn of the rigid body at time interval Δt , is approximated by incremental angles vector, and the incremental angles are estimated using the quadratic spline-approximation as was proposed in [10] – [12]:

$$\delta q(t_i) = \begin{bmatrix} 1 - \frac{1}{12} \|\nabla\theta_i\|^2 \\ \frac{1}{2} \nabla\theta_i - \frac{1}{24} (\nabla\theta_i \times \nabla\theta_{i-1}) \end{bmatrix}, \quad (1)$$

$$\nabla\theta_i = \frac{\Delta t}{12} [5\omega(t_i) + 8\omega(t_{i-1}) - \omega(t_{i-2})].$$

Using (1) and multiplication of the elementary quaternions gives an updated quaternion, from which the Euler angles can be calculated [13]:

$$\begin{aligned}
 q(t_i) &= q(t_{i-1})\delta q(t_i), \\
 \delta q(t_i) &= [\delta q_0(t_i) \quad \delta q_1(t_i) \quad \delta q_2(t_i) \quad \delta q_3(t_i)]^T, \\
 \varphi &= \arctan\left(\frac{2(q_2q_3 + q_0q_1)}{q_0^2 - q_1^2 - q_2^2 + q_3^2}\right), \\
 \theta &= \arcsin(-2(q_1q_3 - q_0q_2)), \\
 \psi &= \arctan\left(\frac{2(q_1q_2 + q_3q_0)}{q_0^2 + q_1^2 - q_2^2 - q_3^2}\right).
 \end{aligned} \tag{2}$$

The specific forces are transformed in the navigation frame by means of updated quaternion and are corrected to gravitational and centripetal accelerations [13], [14]

$$\tilde{a} = q \otimes a_m^{body} \otimes q^* + g - \Omega \times \Omega \times r, \tag{3}$$

where q^* is a complex conjugate of q .

Velocity and position are calculated using an approximation similar to the one used for incremental angles calculation [13]:

$$\begin{aligned}
 v(t_i) &= v(t_{i-1}) + (5\tilde{a}(t_i) + 8\tilde{a}(t_{i-1}) - \tilde{a}(t_{i-2})) \cdot \frac{\Delta t}{12}, \\
 r(t_i) &= r(t_{i-1}) + (3\tilde{a}(t_i) + 10\tilde{a}(t_{i-1}) - \tilde{a}(t_{i-2})) \\
 &\quad \cdot \frac{\Delta t^2}{24} + \Delta t \cdot v(t_{i-1}).
 \end{aligned} \tag{4}$$

Such estimation of velocity and position significantly decreases computational workload. Expressions (1) – (4) represent the algorithm of a functioning integrated system.

The inertial navigation system is corrected from GNSS receiver, magnetometer, and barometric altimeter using Kalman filtering equations. Vector of INS errors is defined as: μ is an orientation error, $\delta v, \delta r$ are the vectors of velocity and position calculation errors. To save the place, the full derivation of the used equations is not given here. More details can be found in [13], [15], [16]. The correction task is solved as:

$$\hat{\mathbf{x}}_k = \bar{\mathbf{x}}_k + \mathbf{K}_k (\mathbf{z}_k - \mathbf{H}\bar{\mathbf{x}}_k), \quad \bar{\mathbf{x}}_{k+1} = \Phi_k \hat{\mathbf{x}}_k, \tag{5}$$

In addition to (5), Kalman filtering equations to provide the vector of the optimal estimate $\hat{\mathbf{x}}_k$ are:

$$\begin{aligned}
 K_k &= P_k(-)H^T (HP_k(-)H^T + R_k)^{-1}, \\
 P_{k+1}(-) &= \Phi_k P_k(+) \Phi_k^T + Q_k^T, \\
 P_k(+) &= P_k(-) - K_k (HP_k(-)H^T + R_k) K_k^T,
 \end{aligned} \tag{6}$$

matrices Q_k, R_k in (6) are the covariance matrices of errors in INS error propagation equation and measurement equation. Features of designing guidance and control systems are represented in [17] – [20].

III. EXPERIMENTAL VALIDATION

A. Description of experiment set up and equipment used

A flight test was performed in October in Kyiv. Weather conditions were the following: cloudy, air temperature about 8 C, humidity about 80 %, wind-south-west, about 2 m/s.

In the presented experiment the task was to fly along the piecewise linear trajectory specified by 8 waypoints (Fig. 1). Sections WP1-WP2, WP5-WP6, WP6-WP7, WP7-WP8, WP8-WP1 are straight-line segments that has to be flown with a constant speed 5 m/s and a relative height 50 m. Section WP2-WP3 has to be performed with smooth descent from 50 to 30 m, WP3-WP4 – is a straight-line segment that has to be flown at a relative height 30 m with a constant speed 5 m/s, WP4-WP5 – a smooth climb from 30 to 50 m. The task was to fly along the given spatial trajectory 3 times, which was successfully performed by the control system.

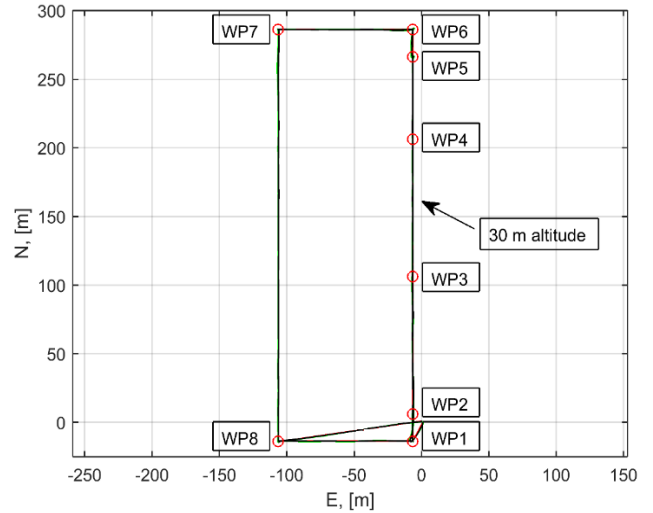


Fig. 1. Experimental trajectory of a quadrotor in the horizontal plane

The equipment used for experimental research (Figs. 2 and 3): quadrotor, designed experimental sample of integrated navigation, guidance and control system, double-frequency GNSS receivers "rover" and "base", GNSS antennas

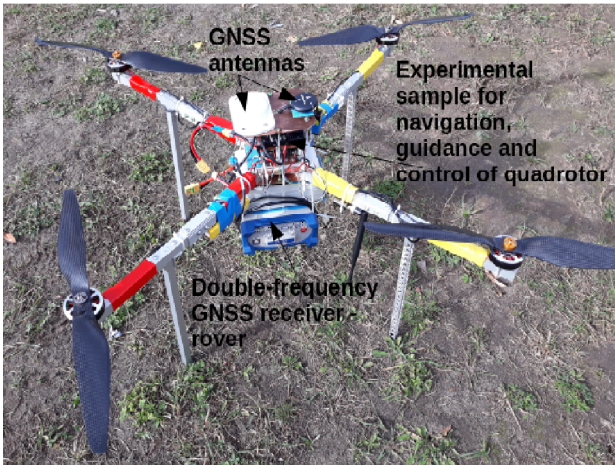


Fig. 2. Photo of drone and used equipment

The represented aids have been allowed to carry out the experimental research of the integrated navigation, guidance and control system.



Fig. 3. Photo of GNSS equipment used for construction in post-processing of the reference trajectory: antenna and double-frequency receiver

B. Results of Experiment

In Figure 4, the enlarged fragments of the experimental trajectory of the quadrotor in the horizontal plane around waypoints WP4 and WP6 is shown. It appears that while moving along a straight line, the deviation of the quadrotor from a given trajectory was not more than 30 cm (WP4). However, we may observe so-called "loop" around WP6, which was caused by the fact that the quadcopter flew over point 4, and to return back to

the trajectory, made a maneuver "loop". The same thing happened when turning at point WP6. Deviations from the specified trajectory were not more than 1.5 m, which is a pretty good result.

In Figures 5 and 6, the values of coordinates and velocity components in the local topocentric coordinate frame during the experiment are presented. The following color designations are accepted here: red – specified reference values, green – actually performed obtained from single GNSS, black – actually performed obtained from the integrated navigation system.

Figure 7 presents the values of relative altitude during the experiment from three sources: GNSS only (green line), barometric altimeter (blue line) and, the integrated navigation system (black line). It can also be seen that the relative altitude obtained from the integrated navigation system is more accurate and smoother compared to the ones obtained separately from GNSS and barometric altimeter.

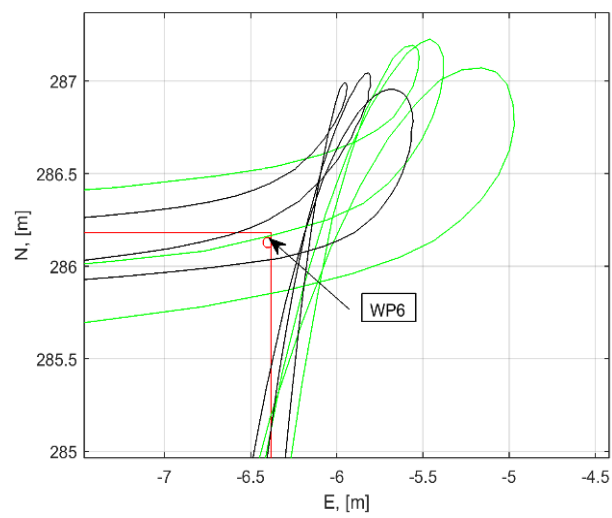
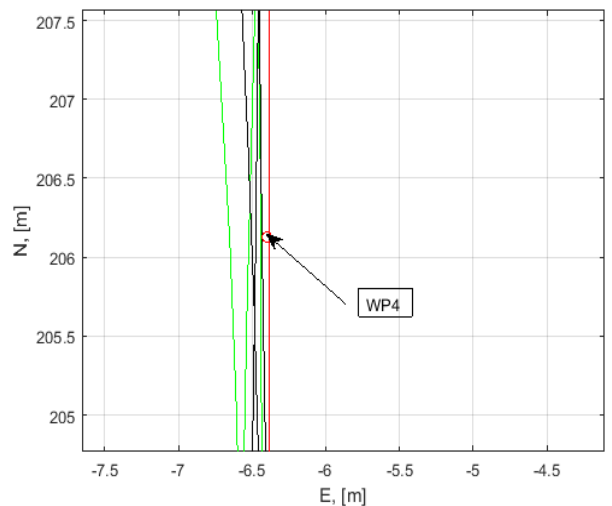


Fig. 4. Enlarged fragments of the experimental trajectory of drone in the horizontal plane: waypoints WP4 and WP6

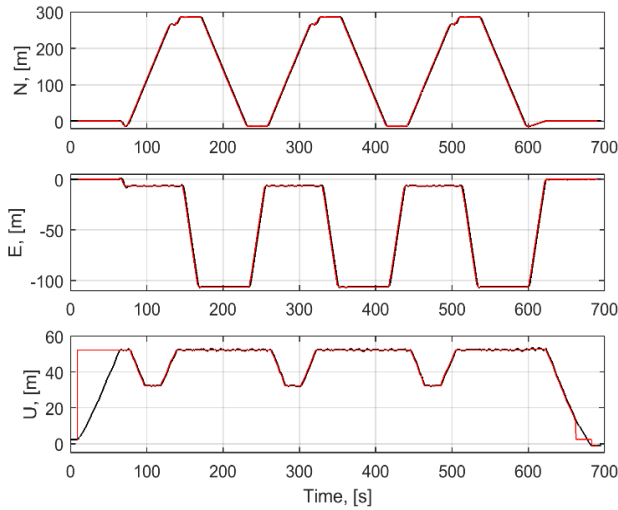


Fig. 5. Coordinates in the local topocentric coordinate frame: North, East, Up.

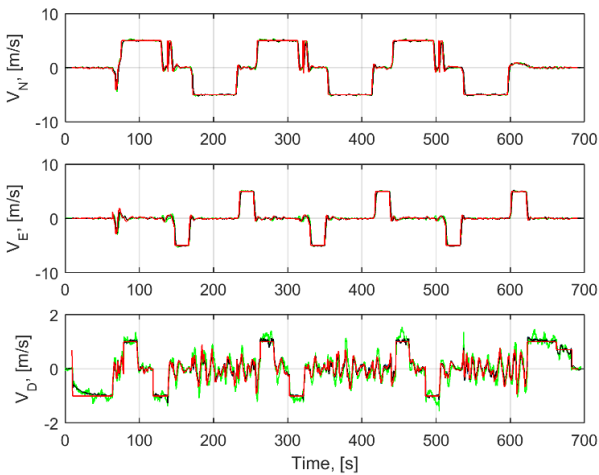


Fig. 6. Components of velocity: North, East, Down

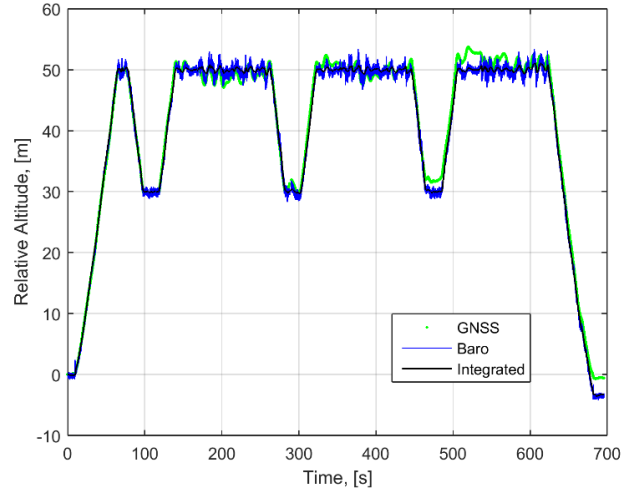


Fig. 7. Components of velocity: North, East, Down

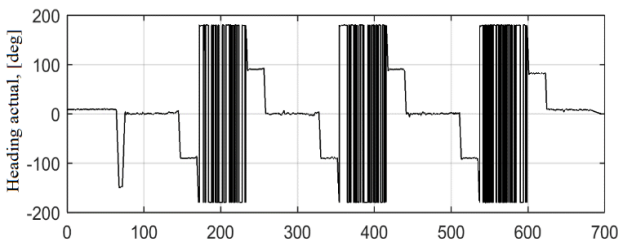
In Figures 8 – 10, the specified and actual values of heading, roll and pitch angles are presented.

The upper parts of the figures correspond to the actual obtained values during whole experiment, and the lower parts correspond to scaled angle's values for the timeframe [252–263 s] timeframe of experiment.

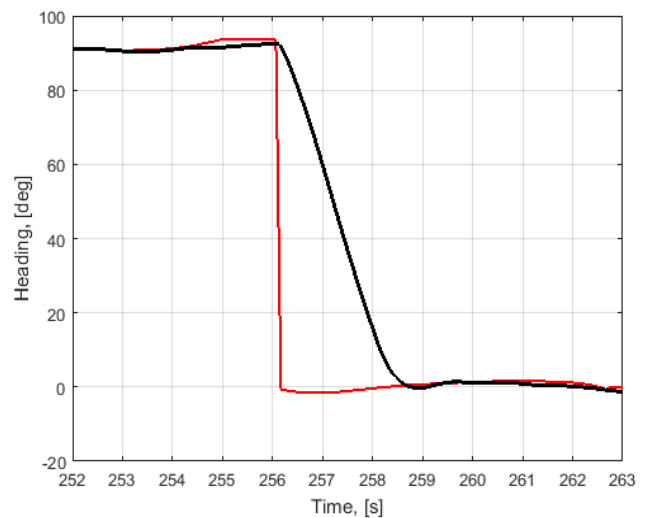
During this time interval there was a change of heading from 90° to 0° . It appears that changing the heading by 90° requires about 4–5 s.

Also, heading change of the quadrotor requires to perform appropriate oscillating maneuvers for the roll and pitch angles.

We may see that in general the autopilot system worked out the set values quite accurately. The actual values of roll and pitch angles were mostly within $\pm 10^\circ$ and $\pm 20^\circ$ correspondently.



a)



b)

Fig. 8. Heading: (a) during whole experiment; (b) scaled for timeframe (252–263 s)

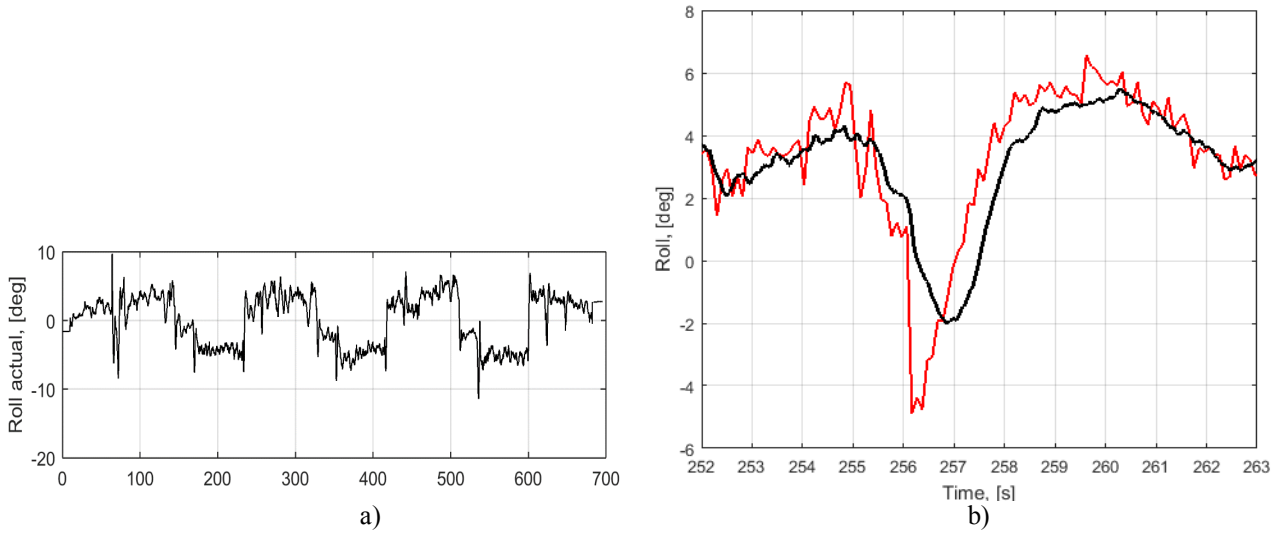


Fig. 9. Roll: (a) during whole experiment; (b) scaled for timeframe (252–263 s)

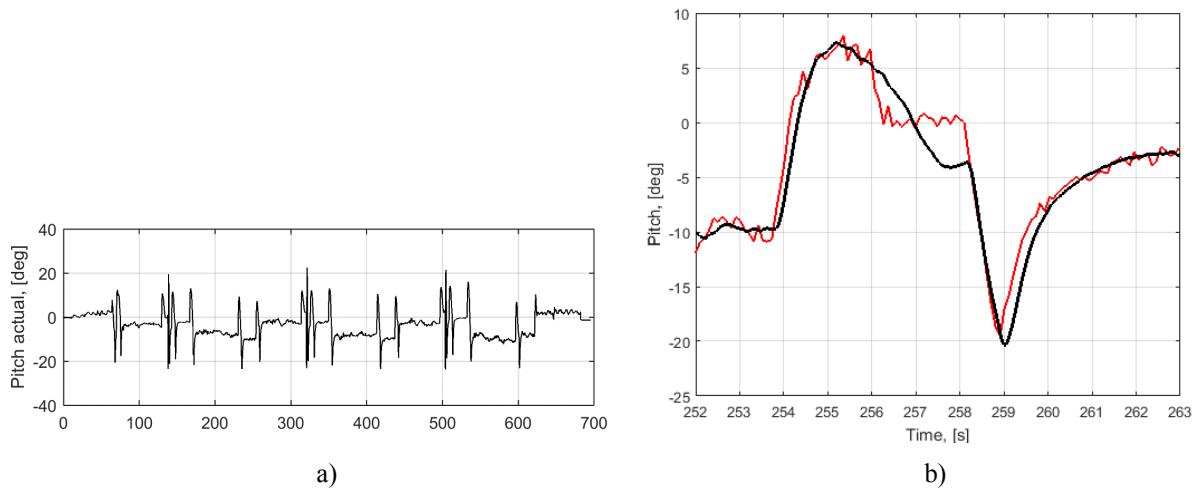


Fig. 10. Pitch: (a) during whole experiment; (b) scaled for timeframe (252–263 s)

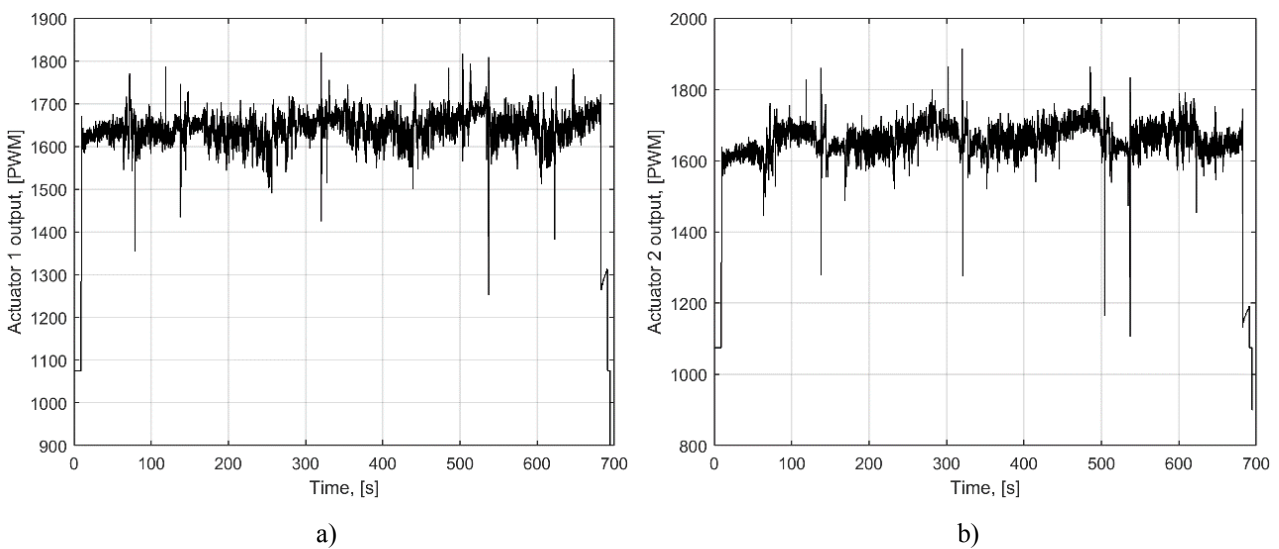


Fig. 11. Pulse width modulation signals of actuators: (a) – (d) – for 1st, 2nd, 3rd, 4th actuators respectively

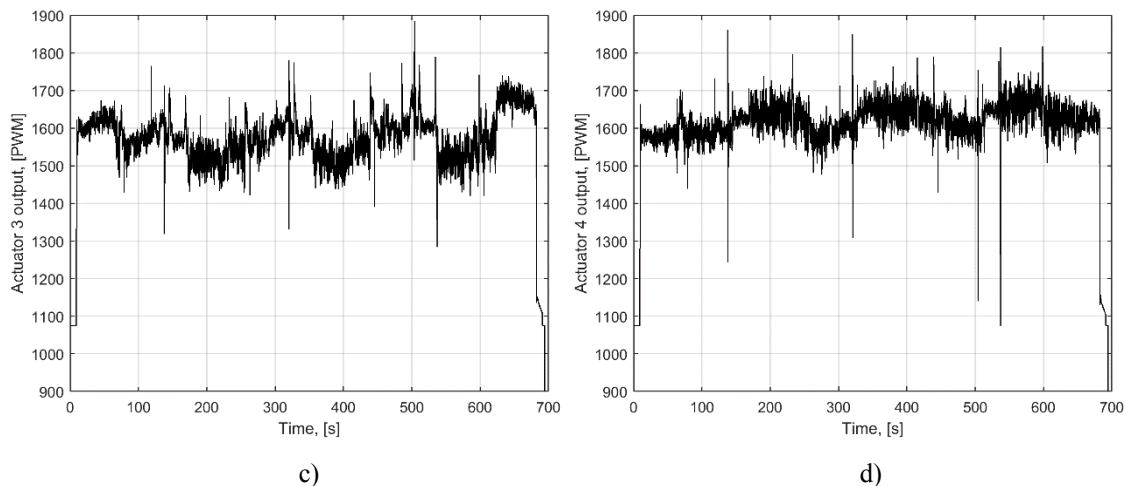


Fig. 11. Ending. (See also p. 84)

Figure 11 presents the values of pulse width modulation (PWM) signals supplied separately for each actuator. We see that the PWM values were in the range of 900–1900. These limits may vary slightly depending on the settings of the control panel.

IV. CONCLUSIONS

The actual values of roll and pitch angles were mostly within $\pm 10^\circ$ and $\pm 20^\circ$ correspondently, which corresponds to quite safe and reliable mode.

We can conclude that the autopilot worked quite well, despite the noise in the sensors.

The represented results can be considered as components of the system analysis directed to improving quality of designing navigation and control system of the quadrotor.

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Kondratiuk Vasyl. ORCID 0000-0002-5690-8873. Candidate of Sciences (Engineering). Senior researcher. Research and Training Centre "Aerospace Centre," National Aviation University, Kyiv, Ukraine. Education: Kyiv Polytechnic Institute, Kyiv, Ukraine, (1985). Research area: global navigation satellite systems, unmanned aerial vehicles, data transmission systems. Publications: 70. E-mail: kon_vm@ukr.net.

Ilnytska Svitlana. ORCID 0000-0003-2568-8262. Candidate of Science (Engineering). Senior Researcher. Research and Training "Aerospace Centre," National Aviation University, Kyiv, Ukraine. Education: National Aviation University, Kyiv, (2007). Research area: navigation and control, integrated navigation systems, satellite and inertial navigation systems, sensor calibration technologies, computer simulation. Publications: 45. E-mail: ilnytskasv84@gmail.com

Kutsenko Oleksandr. ORCID 0000-0003-2741-5559. Candidate of Science (Engineering). Senior Researcher. Research and Training Centre "Aerospace Centre," National Aviation University, Kyiv, Ukraine. Research area: satellite radio navigation, satellite landing system, computer simulation, programming, microcontrollers, program radio. E-mail: kutsenco@bigmir.net

Sushchenko Olha. ORCID 0000-0002-8837-1521. Doctor of Engineering. Professor. Faculty of Air Navigation, Electronics and Telecommunications, National Aviation University, Kyiv, Ukraine. Education: Kyiv Polytechnic Institute, Kyiv, Ukraine, (1980). Research area: systems for stabilization of information-measurement devices. Publications: 250. E-mail: sushoa@ukr.net

Kondratiuk Maryna. ORCID 0000-0003-3376-4800. Researcher. Research and Training Centre "Aerospace Centre," National Aviation University, Kyiv, Ukraine. Education: National Technical University of Ukraine "Ihor Sikorsky Kyiv Polytechnic Institute", Kyiv, Ukraine (2010). Research area: drone navigation systems, computer modeling, programming

Publications: 12.

E-mail: kondratyukmv@gmail.com

Semenenko Oleksandra. ORCID 0000-0003-3184-8170. Junior Research.

Research and Training Centre "Aerospace Centre," National Aviation University, Kyiv, Ukraine.

Education: National Technical University of Ukraine "Igor Sikorsky Kyiv Polytechnic Institute", Kyiv, Ukraine (2012).

Field of scientific activity: satellite radio navigation, computer modeling

E-mail: sashka_com@ukr.net

В. М. Кондратюк, С. І. Ільницька, О. В. Куценко, О. А. Сущенко, М. В. Кондратюк, О. В. Семененко.
Експериментальне дослідження інтегрованих навігаційних систем в задачах відстеження траєкторій квадрокоптерів

У статті представлено результати експериментальних досліджень інтегрованої системи навігації, наведення та керування квадрокоптера. Представлені математичні основи дослідження системи. Представлено алгоритм функціонування інтегрованої системи. Наведено рівняння оптимального оцінювання. Описано особливості експериментального обладнання. Змодельована траєкторія квадрокоптера в горизонтальній площині. Досліджено координати топоцентричної системи координат. Наведено результати експериментальних досліджень. Представлені компоненти швидкості. Наведено графічні залежності кутів ризику, тангажу та крену. Отримані результати можуть бути корисними для створення перспективних навігаційних систем для квадрокоптерів. Вони дозволяють підвищити якість їх навігації.

Ключові слова: глобальна навігаційна супутникова система; інерціальна навігаційна система; система наведення та управління; квадрокоптер; експериментальні дослідження; льотні випробування.

Кондратюк Василь Михайлович. ORCID 0000-0002-5690-8873. Кандидат технічних наук. Старший науковий співробітник.

Науково-навчальний центр «Аерокосмічний центр», Національний авіаційний університет, Київ, Україна.

Освіта: Київський політехнічний інститут, Київ, Україна, (1985).

Напрямок наукової діяльності: глобальні навігаційні супутникові системи, безпілотні літальні апарати, системи передачі даних.

Кількість публікацій: 70.

E-mail: kon_vm@ukr.net

Ільницька Світлана Іванівна. ORCID 0000-0003-2568-8262. Кандидат технічних наук. Старший науковий співробітник.

Науково-навчально центр «Аерокосмічний центр», Національний авіаційний університет, Київ, Україна.

Освіта: Національний авіаційний університет, Київ, (2007).

Напрямок наукової діяльності: навігація та управління, інтегровані навігаційні системи, супутникові та інерціальні навігаційні системи, технології калібрування датчиків, комп'ютерне моделювання

Кількість публікацій: 45.

E-mail: ilnytskasv84@gmail.com

Куценко Олександр Вікторович. ORCID 0000-0003-2741-5559. Кандидат технічних наук. Старший науковий співробітник.

Науково-навчальний центр «Аерокосмічний центр», Національний авіаційний університет, Київ, Україна.

Напрямок наукової діяльності: супутникова радіонавігація, супутникові системи посадки, комп'ютерне моделювання, програмування, мікроконтролери, програмне радіо.

E-mail: kutsenco@bigmir.net

Сущенко Ольга Андріївна. ORCID 0000-0002-8837-1521. Доктор технічних наук. Професор.

Факультет аеронавігації, електроніки та телекомунікацій, Національний авіаційний університет, Київ, Україна.

Освіта: Київський політехнічний інститут, Київ, Україна, (1980).

Напрямок наукової діяльності: системи стабілізації інформаційно-вимірювальних пристроїв.

Кількість публікацій: 250.

E-mail: sushoa@ukr.net

Кондратюк Марина Василівна. ORCID 0000-0003-3376-4800. Науковий співробітник.

Науково-навчальний центр «Аерокосмічний центр», Національний авіаційний університет, Київ, Україна.

Освіта: Національний технічний університет України «Київський політехнічний інститут імені Ігоря Сікорського», Київ, Україна, (2010).

Напрямок наукової діяльності: системи навігації дрона, комп'ютерне моделювання, програмування.

Публікації: 12.

E-mail: kondratyukmv@gmail.com

Семененко Олександра Василівна. ORCID 0000-0003-3184-8170. Молодший науковий співробітник.

Науково-навчальний центр «Аерокосмічний центр», Національний авіаційний університет, Київ, Україна.

Освіта: Національний технічний університет України «Київський політехнічний інститут імені Ігоря Сікорського», Київ, Україна, (2012).

Напрямок наукової діяльності: супутникова радіонавігація, комп'ютерне моделювання.

E-mail: sashka_com@ukr.net